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PCT

NOTIFICATION OF TRANSMITTAL OF THE INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Rule 71.1)

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IMPORTANT NOTIFICATION

International application No.

PCT/DK99/00102

International filing date (day/month/year)

03/03/1999

Priority date (day/month/year)

03/03/1998

Applicant

TOCCATA TECHNOLOGY et al.

1. The applicant is hereby notified that this International Preliminary Examining Authority transmits herewith the international preliminary examination report and its annexes, if any, established on the international application.
2. A copy of the report and its annexes, if any, is being transmitted to the International Bureau for communication to all the elected Offices.
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INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Article 36 and Rule 70)

Applicant's or agent's file reference P 98 001 WO	FOR FURTHER ACTION See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/416)	
International application No. PCT/DK99/00102	International filing date (day/month/year) 03/03/1999	Priority date (day/month/year) 03/03/1998
International Patent Classification (IPC) or national classification and IPC H03F3/217		
Applicant TOCCATA TECHNOLOGY et al..		

1. This international preliminary examination report has been prepared by this International Preliminary Examining Authority and is transmitted to the applicant according to Article 36.



2. This REPORT consists of a total of 5 sheets, including this cover sheet.

☒ This report is also accompanied by ANNEXES, i.e. sheets of the description, claims and/or drawings which have been amended and are the basis for this report and/or sheets containing rectifications made before this Authority (see Rule 70.16 and Section 607 of the Administrative Instructions under the PCT).

These annexes consist of a total of 9 sheets.

3. This report contains indications relating to the following items:

- I ☒ Basis of the report
- II ☐ Priority
- III ☐ Non-establishment of opinion with regard to novelty, inventive step and industrial applicability
- IV ☐ Lack of unity of invention
- V ☒ Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
- VI ☐ Certain documents cited
- VII ☐ Certain defects in the international application
- VIII ☐ Certain observations on the international application

Date of submission of the demand 06/09/1999	Date of completion of this report 11.05.2000
Name and mailing address of the international preliminary examining authority:  European Patent Office D-80298 Munich Tel. +49 89 2399 - 0 Tx: 523656 epmu d Fax: +49 89 2399 - 4465	Authorized officer Dietsche, S Telephone No. +49 89 2399 7465 

**INTERNATIONAL PRELIMINARY
EXAMINATION REPORT**

International application No. PCT/DK99/00102

I. Basis of the report

1. This report has been drawn on the basis of (*substitute sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this report as "originally filed" and are not annexed to the report since they do not contain amendments.*):

Description, pages:

7-13 as originally filed

1-6 as received on 02/05/2000 with letter of 27/04/2000

Claims, No.:

1-12 as received on 02/05/2000 with letter of 27/04/2000

Drawings, sheets:

1/6-6/6 as originally filed

2. The amendments have resulted in the cancellation of:

- ☐ the description, pages:
☐ the claims, Nos.:
☐ the drawings, sheets:

3. ☐ This report has been established as if (some of) the amendments had not been made, since they have been considered to go beyond the disclosure as filed (Rule 70.2(c)):

4. Additional observations, if necessary:

**INTERNATIONAL PRELIMINARY
EXAMINATION REPORT**

International application No. PCT/DK99/00102

V. Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

1. Statement

Novelty (N)	Yes:	Claims	1-12
	No:	Claims	
Inventive step (IS)	Yes:	Claims	1-12
	No:	Claims	
Industrial applicability (IA)	Yes:	Claims	1-12
	No:	Claims	

2. Citations and explanations

see separate sheet

1. The following document will be referred to in this report:

D1 = US-5 410 592

2. With respect to item V, the examiner is of the provisional opinion that the subject-matter of the independent claims 1 and 7 and of the dependent claims 2-6 and 8-12 meets the requirements of Art. 33 (2) (3) and (4) PCT.

- 2.1 D1 which is considered to represent the state of the art the closest to the present application discloses in the description (col. 1, line 61 to col. 4, line 47) and in the drawings (fig. 1 and 2) a class D audio amplifier with a specific feed-back network which produces an error signal that is combined with the audio input signal to form an error compensated audio signal applied to a pulse-width modulator.

The method claimed in claim 1 differs from this prior art document in that

- the error signal is detected by detecting deviations between the pulse-widths of the pulse-width modulated great-signal and the pulse-width modulated small-signal, and in that
- the detected error signal is used to control a carrier signal applied to the pulse-width modulator, in order to minimize the detected error.

Since this "method in the compensation of distortions in an amplifier which are generated by non-linearities of the amplifier", as claimed in present claim 1, is neither known from, nor rendered obvious by any available prior art document, the subject-matter of claim 1 is considered to meet the requirements of Art. 33 (2) (3) and (4) PCT.

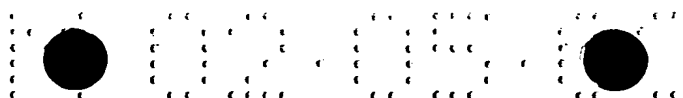
- 2.2 Since the subject-matter of present claim 1 appears to meet the requirements of Art. 33 (2) (3) and (4) PCT, the subject-matter of the claims 2-6 depending on claim 1 would also meet the requirements of Art. 33 (2) (3) and (4) PCT.

- 2.3 For the same reasoning as elaborated above (point 2.1) with respect to the subject-matter of the independent method claim 1, the subject-matter of the corresponding independent apparatus claim 7 is also considered to meet the requirements of Art. 33 (2) (3) and (4) PCT.

**INTERNATIONAL PRELIMINARY
EXAMINATION REPORT - SEPARATE SHEET**

International application No. PCT/DK99/00102

- 2.4 Since the subject-matter of present claim 7 appears to meet the requirements of Art. 33 (2) (3) and (4) PCT, the subject-matter of the claims 8-12 depending on claim 7 would also meet the requirements of Art. 33 (2) (3) and (4) PCT.



1

A method in the compensation of nonlinearities in an amplifier, an amplifier, and uses of the method and the amplifier

5

The invention relates to a method in the compensation of distortions in an amplifier which are generated by nonlinearities of the amplifier that consists of a pulse-width modulator wherein a signal is pulse-width modulated to provide a pulse-width modulated small-signal, and wherein the pulse-width modulator has an output controlling a set of change-over switches which feed a load with a pulse-width modulated great-signal by means of a voltage supply.

15

The invention moreover relates to an amplifier of the type comprising a pulse-width modulator adapted to pulse-width modulate a signal to provide a pulse-width modulated small-signal, said pulse-width modulated signal being fed to at least two change-over switches adapted to connect and disconnect a voltage supply to form a pulse-width modulated great-signal, and having means to compensate for error signals which occur in the signal paths between the pulse-width modulated great-signal and the pulse-width modulated small-signal.

Finally, the invention relates to uses of the amplifier.

Traditional amplifiers for audio uses are used for amplifying audio signals and for forming sound images in loudspeakers. These amplifiers, however, do not have very high efficiencies.

Therefore, amplifiers are being designed according to other principles. These high efficiency amplifiers include

de those which are based on pulse-width modulation. These amplifiers are also referred to as class D amplifiers. Such an amplifier consists of a pulse-width modulator, a set of change-over switches and a low-pass filter.

5 The principle of a class D amplifier is that two change-over switches are switched to conduct and non-conduct, respectively, depending on the amplitude of a signal, such as an audio signal. The information of the audio
10 signal is hereby converted into a series of pulses whose width corresponds closely to the information of the audio signal.

Instead of two change-over switches, it is possible to
15 use four change-over switches which are caused to conduct and non-conduct in pairs.

Pulse-width modulated amplifiers are theoretically very linear and thereby have a very low distortion, but practical realizations have shown that nonlinearities are unfortunately formed in these amplifiers, which has prohibited the use of these as High Fidelity amplifiers unless strong negative feedback systems have been established.

25 However, establishment of feedback systems in pulse-width modulated amplifiers is not an easy task, since negative feedback performed prior to the low-pass filtering causes much noise in the system.

30 Furthermore, the load impedance, which is a loudspeaker, is incorporated in the design of the feedback system, and since this impedance may vary depending on loudspeaker selection, the design is thus impeded by the feedback system.

35

A great part, but not an exclusive part, of the unlinearities in pulse-width modulated amplifiers occurs because the voltage supply to the change-over switches is not constant in the operation of the amplifier.

5 The reason is that the gain in pulse-width modulated amplifiers is derived from the supply voltage to the change-over switches incorporated in the amplifier, divided by the peak voltage of the carrier wave, which is typically a saw-toothed or triangular signal. The gain of the
10 amplifier is thus proportional to the supply voltage, so that variations in it cause a so-called multiplicative error to occur on the output signal from the change-over switches.

15 A regulated voltage supply may be used to eliminate unlinearities, but a very complex power supply circuit is required for sufficiently linear properties to be achieved, which adds considerably to the costs of the amplifier.

20

Moreover, it is known that the dead time, which is the time where none of the change-over switches is made, causes distortion of the amplified signal.

25 It is therefore desirable to reduce the dead time to a minimum in pulse-width modulated power amplifiers. Conversely, less dead time causes problems of increased power consumption and strong ringing on the output signal, because both change-over switches carry current from
30 the supply directly down into earth.

The known methods of linearizing pulse-width modulated amplifiers require strong negative feedback, as mentioned. These methods are particularly unuseful for consumer amplifiers, where design criteria such as low com-
35

plexity and general usefulness in a broad range of load are important.

5 EP O 503 571 A1 discloses a class D amplifier in which variations in the voltage supply are compensated by changing the carrier wave signal as a function of an error in the voltage supply.

10 Finally US A 5 410 592 discloses a class D ampflfier with a specifik feed-back network which produces an error signal that is combined with the audio input signal to form an error compensated audio signal applied to a pulse-width modulator.

15 On the other hand, other errors that may cause errors in the pulse widths of the pulse-width modulated great-signal will not be included in the compensation.

20 Accordingly, an object of the invention is to provide a method which is capable of linearizing and compensating for all errors which occur between the signal paths of a pulse-width modulated small-signal and a pulse-width modulated great-signal.

25 The object of the invention is achieved by the method defined in the introductory portion of claim 1 which is characterized in that the inevitable error, which manifests itself in that the pulse widths of the pulse-width modulated great-signal differ from the pulse widths of
30 the pulse-width modulated small-signal, is detected as an error signal by detecting deviations between the pulse-widths of the modulated great-signal and the pulse-width modulated small-signal, wherein the detected error signal is used to control a carrier signal to the pulse-width
35 modulator.

AMENDED SHEET

When, as stated in claim 2, the error signal is detected as a multiplicative error signal, it is relatively easy to modulate the carrier wave signal as a function of the
5 multiplicative error signal.

As stated in claim 3, the detected multiplicative error signal is determined as a signal which is established as a signal between the pulse-width modulated small-signal multiplied by the pulse-width modulated great-signal and the inverted small-signal multiplied by the inverted pulse-width modulated great-signal.
10

A further circuit-technical advantage is achieved hereby as the compensating circuit both compensates for the multiplicative errors in the pulse width and additionally for the pulse height that occurs in the change-over switches. In addition, a simple implementation of the invention is achieved.
15

It is noted that the method is particularly suitable for compensating for multiplicative errors in an H-bridge which is operated in class AD operation.
20

Expediently, as stated in claim 4, the pulse-width modulation is performed by means of a carrier wave signal, which is particularly expedient for use in the pulse-width modulation of analogue signals, when the carrier wave signal is analog.
25

It is however also possible to use a carrier wave signal that is digital.

30

For simple circuit design of the pulse-width modulation, it is an advantage if, as stated in claim 5, a sawtoothed or triangular carrier wave signal is used.

35 When, as stated in claim 6, the slew rate of the carrier wave is adjusted by an external signal, it is ensured

that the gain of the compensated amplifier may be varied over a great range.

As mentioned, the invention also relates to an amplifier.

5 This amplifier is characterized in that the means for compensating for the error signals are formed by a detector adapted to detect deviations between the pulse widths of the great-signal and of the pulse-width small-signal, and that the output of the detector is connected to a controlled carrier wave generator.

10 An amplifier is hereby provided in which inevitable nonlinearities, which manifest themselves by differences between the pulse-width modulated small-signals and the pulse-width modulated great-signals, may be eliminated without complicated feedback stages.

15 Expedient embodiments of the amplifier are defined in claims 8-10.

20 Finally, the invention relates to uses of the method and the amplifier, as mentioned.

25 The use according to claim 11 allows a much simpler structure to be provided than the negative feedbacks traditionally used in pulse-width modulated amplifiers.

30 The use according to claim 12 allows the amplifier to be used for the control of resistive and reactive loads, which are e.g. found in electric motors, physical laboratory equipment, measuring apparatus, etc.

35 The invention will now be explained more fully with reference to an embodiment of the invention shown in the drawing, in which

AMENDED SHEET

P a t e n t C l a i m s :

1. A method in the compensation of distortions in an
5 amplifier which are generated by non-linearities of the
amplifier that consists of a pulse-width modulator (4),
wherein a signal is pulse-width modulated to provide a
pulse-width modulated small-signal (5), and wherein the
pulse-width modulator (4) has an output controlling a set
10 of change-over switches (6) which feed a load (9) with a
pulse-width modulated great-signal (7) by means of a
voltage supply (12), c h a r a c t e r i z e d in that
the inevitable error, which manifests itself in that the
pulse widths of the pulse-width modulated great-signal
15 (7) differ from the pulse widths of the pulse-width modu-
lated small-signal (5), is detected as an error signal by
detecting deviations between the pulse-width of the
modulated great-signal and the pulse-width modulated small-
signal, wherein the detected error signal is used to
20 control a carrier signal to the pulse-width modulator.

2. A method according to claim 1, c h a r a c t e r -
i z e d in that the error signal is detected as a multi-
plicative error signal.

25

3. A method according to claim 2, c h a r a c t e r -
i z e d in that the detected multiplicative error signal
is determined as a signal which is established as a
differential signal between the pulse-width modulated
30 small-signal multiplied by the pulse-width modulated
great-signal and the inverted pulse-width modulated small-
signal multiplied by the inverted pulse-width modulated
great-signal.

35 4. A method according to claims 1-3, c h a r a c t e r -

AMENDED SHEET

9. An amplifier according to claim 7 or 8, c h a r a c -
t e r i z e d in that the controllable carrier wave gen-
erator (11) is adapted to keep the frequency of the car-
5 r i e r wave constant.

10. An amplifier according to claims 7-9, c h a r a c -
t e r i z e d in that the controllable carrier wave gen-
erator (11) is adapted to change the slew rate of the
10 c a r r i e r wave on the basis of a detected multiplicative
error signal.

11. Use of a method and an amplifier according to claims
1-10 in a negative feedback system.

15

12. Use of a method and an amplifier according to claims
1-10 for the power control of resistive and reactive
loads.

20

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